

The Effect of Vacuum Impregnation Pretreatment on Air-Drying Kinetics of Pears

Şeyma Uysal^{1,a}, Fikret Pazır^{1,b,*}

¹Engineering Faculty, Food Engineering Department, Ege University, 35040 Izmir, Turkey, *Corresponding author

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Research Article	The aim of this study was to examine the drying kinetics of pears (<i>Pyrus communis L.</i>) with and without vacuum impregnation and under the different temperature by using tray dryer. Vacuum
Received : 17/01/2019 Accepted : 11/09/2020	impregnation were applied to the the pears (15 mm thickness, 65 mm outer and 20 mm inner dimensions respectively) with the conditions of 50° Brix impregnation solution concentration, 225 mbar vacuum pressure and 45 min vacuum time. Drying process was carried out at temperatures of 55, 65 and 75°C. Drying time of non-vacuum impregnated pears was determined 640, 500 and 340 min and vacuum impregnated pears was determined 700, 540 and 560 min respectively. Page, Exponential, Henderson and Pabis, Diffusion Approach were examined for testing the drying like the current values resulted pears and the current values results of the current values results
<i>Keywords:</i> Vacuum Pretreatment Drying Drying Time Drying Kinetics Pear	kinetics. Experimental values are in accordance with the expected values resulted Page and Difussion models of with and without vacuum impregnated pears. Effective diffusion coefficient (D_{eff}) was varying 2.74×10^{-11} to 7.31×10^{-11} m ² /s. m ² /s with respect to the drying temperatures. The activation energy for the non-vacuum impregnated and vacuum impregnated pears was 32.93 kJ / mol and 24.25 kJ / mol, respectively.
a 😒 seymauysal.92@gmail.com 🛛 🕕	https://orcid.org/0000-0001-6271-4752 b fikret.pazir@gmail.com b https://orcid.org/0000-0003-3997-4892

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Introduction

Drying is one of the most commonly used methods of food preservation; in some cases, the quality of products such as fruits and vegetables can be adversely affected. Such as products which are air-dried at high temperatures, lose their rehydration ability. Undesirable changes can occur in colour, texture and flavor because of the high temperatures. Drying can cause to decrease at some of the nutritional ingredients.

In order to prevent drying damages, different pretreatments are applied such as blanching, immersion, osmotic dehydration and vacuum impregnation (Abano and Sam-Amoah, 2011). One of these pretreatments is the vacuum impregnation which is defined as the osmotic dehydration process under vacuum for a certain period of time. The efficiency of the osmotic dehydration process rises throughout the process (Fito and Chiralt, 2000). Vacuum impregnation is usually used as a pre-treatment of the fruit and vegetables. Because, plant tissues can not reach to water activity level being safe for microbial growth (Us, 2006). Moreover, if vacuum impregnation is combined with air-drying, freezing, freze drying, microwave drying, microwave vacuum drying, vacuum drying it is possible to make a wide range of natural functional products (Betoret et al., 2003; Fito et al., 2001; Hironaka et al., 2011; Schulze, 2012; Maran et al., 2013).

The process parameters must be selected appropriately to determine the effects of vacuum impregnation on the physico-chemical properties and sensory properties of the products. There are many parameters that affect the efficiency of the vacuum impregnation process and the final product quality. The parameters in relation to the raw material can be listed as internal factors (Type of raw material, the structure of raw metarial and the surface area, thickness, shape of raw metarial) the process parameters during application can be listed as external factors(vacuum Pressure, vacuum time, restoration time after vacuum (impregnation time at atmospheric pressure), the type of solvent used in the impregnation solution, the molecular weight, concentration of the impregnation solution, ratio of impregnation solution to the food, the temperature of the impregnation solution, stirring).

Drying is also a complicated process which includes both heat and mass transfer (Şahin ve Dinçer, 2005). From the engineering perspective, it is essential to comprehend the control parameters of this complicated process. The mathematical modelling of drying is applied in order to design innovative drying systems, to improve present processes and to control the whole process. Many researchers have developed mathematical models to describe and control drying processes in foodstuffs.

From the point of qualitative and quantitative pomace content of view, pears are considered as the second most important fruits after apple.

The major edible pear species in Turkey is P. communis as well (Öztürk et al., 2009). In this study, the deveci species (Pyrus communis L.), one of the widely grown pear varieties in Turkey, was procured from the local market. The deionized apple juice concentrate was used as the impregnation solution. In order to improve the sensory and quality characteristics of dried pears, it was aimed to impregnate the fruits with their own sugars by using deionized apple juice concentrate instead of sugar derivatives such as sucrose and glucose which are frequently used as impregnation solution during vacuum impregnation process. The deionized apple juice concentrate, consisting of the majority of the sugars was obtained by removing the minerals, phenolic substances and other components as much as possible from the solution.

The aim of this study was to investigate the drying kinetics of vacuum impregnated and non-vacuum impregnated pears. It also intends to test the conformance of mathematical models with the product, to select the model that describes the kinetic behaviour most satisfactorily and to compute the effective moisture diffusivity.

Material and Method

Material

The pears (Deveci (*Pyrus communis L.*)) were purchased from a local market located in İzmir, Turkey and stored (4°C and %80-85 RH) at the Pilot Plant of Ege University Food Engineering Department in İzmir. The raw material to be used in the experiments was sliced at a thickness of 15 mm after being peeled and the core house was removed. The outer and inner diameters of the pears were measured 65 and 20 mm respectively. The pears was blanched for inactivation of polyphenol oxidase enzyme in boiling water. The preliminary tests were performed in order to determine the blanching time. The necessary blanching time was assessed as 5 min as a result of these tests. The deionized apple juice concentrate was used impregnation solution and was purchased from a manufacturer in Turkey.

Method

Vacuum Impregnation Process

The evacuation of the experimental setup were provided by a vacuum oven (Heraeus, VT 5042, Germany) (Figure 1). The deionized apple juice concentrate was used an impregnation solution. The pears were immersed in beakers containing the impregnation solution before vacuum was applied. The optimum condition for vacuum impregnation process (vacuum pressure (200,350,500 mbar), vacuum time (15,30,45 min) and concentration (30,40,50 °Brix) was determined by Desirability method in Response Surface Methodology with the preliminary study. The optimum condition of vacuum impregnation was 50° Brix impregnation solution concentration, 225 mbar vacuum pressure and 45 min vacuum time. The other parameters of vacuum impregnation process were temperature at 35°C (Paes et al., 2008), restoration time at 60 min (Zhao and Xie, 2004) and a ratio of food over solution at (1/5) (w/w) (Erünal, 2010).

Air-Drying Process

Non-vacuum impregnated (blanched pears) and vacuum impregnated pears was dried at laboratory type tray dryer (Weintek, TURKEY) (Figure 2.). The experiments were conducted in the production facility of Ege University Food Engineering Department. The equipment consists of 10 trays, upper and lower pipes, a broiler, a fan, bottom air suction line and a heater. The trays consist of the frames having 30x30x2 cm dimensions with pores of 3x3 mm made of stainless steel. The air flow was parallel to the direction where the trays are placed. The uniform distribution of air over the trays inside the tray dryer was performed by an engine rotating at 10 rpm.



Figure 1. Schematical Diagram Of The Vacuum Impregnation Process



Figure 1 Laboratory Type Tray Dryer (Weintek, TURKEY)

Drying experiments were performed at different temperatures (55, 65 and 75°C). The air velocity was 1 m/s and was kept constant at the process. The weight of pears $200 \pm 4,12$ g were placed into one tray. The datas were recorded after the temperature reached the experimental condition at the drying process. All the data were monitored 20 minutes intervals automatically by the dryer. The drying was going on the moisture content of the product became 15%.

Moisture Analyses

The moisture analysis of the pears were carried out in a vacuum oven (WiseVen WOW-30, Germany) at 65°C. The moisture content of non-vacuum impregnated and vacuum impregnated pears were 83.5±0.5 and %71.4±1.2 respectively.

Examination of Drying Kinetics

The most widely used method to measure effective moisture diffusivity is experimentally from drying curves based on the solution of Fick's second law equation. Assuming a constant diffusion coefficient, Fick's equation with one-dimensional diffusion for different geometries slab, cylinder and sphere) can be given as (Srikiatden, 2007)

$$(s\frac{dM}{dt} = D_{eff}(\frac{d^2M}{dx^2} + \frac{\eta}{r}\frac{dM}{dr}) \eta = 0 \text{ for infinite slap}$$
(1)

The assumptions of the diffusion equation for mass transport of initial and boundary conditions:

1. The diffusion coefficient of a pear slices is constant and not a function of moisture concentration.

2. The pear slices is considered isothermal and heat transfer is neglected.

3. The pear slices composition is homogeneous and isotropic.

4. The volume change of the pear slices is negligible during the tempering process.

5. Drying takes place in decreasing speed period.

6. The shape factor (ϕ) = 0.493 and the calculation is considered as infinite slap due to the lack of similarity to the cylinder, sphere and cube. The geometry of the pear slices is considered as a infinite slap.

7. Mass transfer takes place in one dimension.

The convective boundary conditions of Fick's 2nd law for homogeneous moisture distribution and symmetrical distribution in the center are as follows(Srikiatden, 2007);

 $M(r,0)=M_i$, t=0 (initial condition) $M(0,t)=M_{\infty}$ r=r₀(at the surface) $M(0,t) = M_{\infty} r = 0$ (at the center)

Equation 2 was obtained when a solution was made according to these conditions.

$$MR = \frac{M_0 - M_{\infty}}{M_t - M_{\infty}} = \frac{8}{\pi^2} \sum_{n=0}^{\infty} \frac{1}{(2n+1)^2} \exp\left[-\frac{(2n+1)^2 \pi^2}{4L^2} D_{eff} t\right] (2)$$

MR : Moisture Ratio.

- M₀ :Initial Moisture Content,
- M_e : Equibrium Moisture Content,
- M_t : Moisture Content at t time.

Under the conditions where the relative humidity and ambient temperature inside the tray dryer do not come to a steady state, the following assumption can be made. The final moisture content of the product is not equal to the equilibrium moisture content. Hence, equilibrium moisture content (M_e) is negligible.

$$MR = \frac{M_0}{M_t} = \frac{8}{\pi^2} \left(e^{\left(\frac{\pi}{2}\right)^2 N_{F_i}} + \frac{1}{9} e^{-9\left(\frac{\pi}{2}\right)^2 N_{F_i}} + \frac{1}{25} e^{-25\left(\frac{\pi}{2}\right)^2 N_{F_i}} \right)$$
(3)

Terms 2 and 3 of Equation 3 are neglected for longterm drying (Fo>0.2). Equation 3 was rewritten only with first term (Equation 4).

$$MR = \frac{M_0}{M_t} = \frac{8}{\pi^2} \left(e^{\left(\frac{\pi}{2}\right)^2 N_{F_i}} \right)$$

$$N_{F_i} = D_{ef} t / L^2$$
(4)

$$N_{Fi} = D_{eff}t/L^{2}$$
$$MR = \frac{M_{0}}{M_{t}} = \frac{8}{\pi^{2}} (e^{-(\frac{\pi}{2})^{2} D_{eff}t/L^{2}})$$

N_{Fi} : Fick Constant, D_{eff} : effective diffusion coefficient (m²/s), L

: Thickness of product

The conformance of the experimental data with four empirical model (Table 1) was tested by SPSS 20.0 software and conducting non-linear regression analysis. For each experiment, coefficient of determination (\mathbb{R}^2) , root of square mean error (RMSE) (Equation 5) and reduced chi-square (χ^2) (Equation 6) values were computed respectively. The model with the highest value of coefficient of determination (R²), and the least RMSE and the least reduced chi-square (χ^2) values has been determined as the best model for each experiment with the goodness of fit and minimum standard deviation between expected and observed values (Sun et al., 2007; Lahsasni -1/2

et al., 2004).RMSE =
$$\left[\frac{1}{N}\sum_{i=1}^{N} (MR_{b,i} - MR_{d,i})^2\right]^{1/2}$$

(5)
 $\chi^2 = \sum_{i=1}^{N} \frac{(MR_{d,i} - MR_{b,i})^2}{N-n}$ (6)

MRd, i i. : Experimental value measured in observation,

MRb,i i. : Expected value in observation,

Ν : Number of observations

Ν :The number of the constants in the model.

Calculation of Effective Moisture Diffusivity and Activation Energy

In order to determine the effect of difusion, the difusion that takes place by multi mechanisms simultaneously can be described as one unique term called effective moisture diffusivity (D_{eff}). It is a great importance to calculate the D_{eff} values from the perspective of the drying behaviour and characteristics of the product (Erbay, 2008). The Deff values were found out by plotting the natural logarithm of the fractional moisture ratio (In MR) obtained by the observed drying values versus time and slope of this graph gives the Deff values (Lomauro et al., 1985, Doymaz et al., 2004).

In order to evaluate the effect of temperature on the effective moisture diffusivity the Arrhenius equation (Equation 7) can be used (Lopez et al., 2000; Srikiatden and Roberts, 2006).

$$D_{\rm eff} = D_0 \exp(-\frac{E_a}{RT}) \tag{7}$$

Activation energy (EA) can be calculated by the slope obtained by plotting the graph of natural logarithm of effective moisture diffusivity ($ln(D_{eff})$), versus inversion of temperature (1/T) in 1/K units.

Table 1. Drying kinetics models

Model Name	Model Equation	R
Page	$MR=exp(-kt^n)$	1
Exponential	MR = exp(-kt)	2
Henderson and Pabis	MR=aexp(-kt)	3
Diffusion Approach	MR=aexp(-kt)+(1-a)exp(-kbt)	4

R: References, 1: Uysal et al. (2017), 2: Eren et al. (2008), 3: Koçak et al. (2018), 4: Ertekin and Yaldız (2004)

Results and Discussion

Pear samples were dried until they reached 15% moisture content in the tray dryer. The weight of pear samples were measured at 20 min time intervals automatically by the dryer and the moisture ratio (MR) was calculated according to these datas. The graphs of moisture ratio versus time for non-vacuum impregnated pears and vacuum impregnated pears were shown in Figure 3 and Figure 4, respectively.

When Figure 3 was examined, drying time of non-vacuum impregnated pears at 55,65 and 75°C was determined 640, 500 and 340 min respectively. The drying time was decreased when the drying temperature was increased for non-vacuum impregnated pears. Hence, the shortest drying time (340 min) was occurred at 75°C.

When Figure 4 was examined, drying time of vacuum impregnated pears at 55,65 and 75°C was determined 700, 540 and 560 min, respectively. The drying time was not linearly changed with the drying temperature for the vacuum impregnated pears. The shortest drying time (540 min) was occurred at 65°C. As generally known, drying time was affected from drying temperature. However, for the vacuum impregnated pears, external resistance across the drying was high because of the sugar content especially

at high temperatures. Therefore, drying time of vacuum impregnated pears at 75°C is higher than that for vacuum impregnated pears at 65°C.

Drying time of vacuum impregnated pears were higher than non vacuum impregnated pears at constant temperature. Vacuum impregnated pears had higher sugar content than non-vacuum impregnated pears. There were bonds occurred between sugar and water molecules. Therefore, for removing the same amount of water from the pears, the long drying time was needed. Kaya et al. (2016) was determined the total convective dehydration times of osmo-dehidrated carrot samples at 55°C. The dehydration time was 900 min for osmo-dehidrated carrot samples.

Evaluation of Drying Kinetics

Examination of drying kinetics were performed according to the R², $\chi 2$, RMSE values which were given in Table 2. The model with the highest R² and the lowest $\chi 2$ and RMSE values was selected as the appropriate model. It might be pointed out that two different models (Page and Diffusion Approach) are able to describe the kinetic behaviour of pear samples conveniently.

The Page model was the best fitted model for nonvacuum impregnated pearss dried at 55 and 65 °C. The coeficients of determination (R²) was 1.00 and 0.998, the root of square mean error (RMSE) values was 0.0137 and 0.0196 and the reduced chi-square ($\chi 2$) values were found to be 1.16×10⁻⁶ and 0.0004 for Page model at 55 and 65°C respectively. The best fitted model for non-vacuum impregnated pears dried at 75°C was Diffusion model. R², RMSE and χ^2 values of Diffusion Model were 0.999, 0,0066 and 5.28×10-5, respectively.

The appropriate model for vacuum impregnated pears dried at 55 and 65°C were Diffusion which had R² values of 0.999 and 0.995, RMSE values of 0,0054 and 0.0201 and $\chi 2$ values of 1,297×10⁻⁵ and 0.0004. The Page model was suitable model for the vacuum impregnated pears dried at 75°C. The R², RMSE and χ^2 values of Page model were 0.998, 0.0198 and 0,0002 respectively. Also, Sahin and Ozturk (2015) were performed vacuum impregnation process before air drying of fig samples at 75°C. That study was examined ten different drying model. The best fitted model of vacuum impregnated and non vacuum impregnated fig samples was Weibull distribution model and Verma model respectively.



Figure 3. Experimental moisture ratios (MR) of nonvacuum impregnated pears at different drying temperature



Figure 4. Experimental moisture ratios (MR) of vacuum impregnated pears at different drying temperature

Model Name	Drying	Non-V	acuum Impregr	nated Pears	Vacuum Impregnated Pears			
Would Iname	Temperature (°C)	\mathbb{R}^2	RMSE	χ^2	\mathbb{R}^2	RMSE	χ^2	
	55	1.000	0.0137	1.16×10 ⁻⁵	0.981	0.199	0.0134	
Page	65	0.998	0.0196	0.0004	0.985	0.2072	0.0259	
	75	0.996	0.0214	0.0005	0.998	0.0198	0.0002	
Exponential	55	0.999	0.0221	6.72×10 ⁻⁵	0.932	0.0537	0.0016	
	65	0.998	0.0421	0.0018	0.976	0.0686	0.0038	
	75	0.993	0.0291	0.0009	0.836	0.0704	0.0022	
Handarson va	55	0.999	0.0256	7.42×10 ⁻⁵	0.953	0.0459	0.0005	
Pabis	65	0.998	0.0431	0.0020	0.977	0.0608	0.0031	
	75	0.994	0.0013	0.0013	0.922	0.0577	0.0033	
Diffusion	55	0.999	0.0246	7.16×10 ⁻⁵	0.999	0.0054	1.297×10 ⁻⁵	
	65	0.998	0.0397	0.0017	0.995	0.0201	0.0004	
	75	0.999	0.0066	5.28×10 ⁻⁵	0.986	0.1139	0.0033	

Table 2. Statistical evaluation of drying models for pears (\mathbb{R}^2 , x^2 , RMSE Values)

Table 3. Model coefficients at different drying temperatures for pears

Model Neme	Drying	Non-Vacuum Impregnated Pears			Vacuum Impregnated Pears				
Wodel Mame	Temperature (°C)	k	n	а	b	k	n	а	b
	55	0.003	0.967	-	-	0.005	0.741	-	-
Page	65	0.004	0.969	-	-	0.010	0.871	-	-
	75	0.008	0.921	-	-	0.027	0.607	-	-
Exponential	55	0.003	-	-	-	0.002	-	-	-
	65	0.004	-	-	-	0.002	-	-	-
	75	0.006	-	-	-	0.003	-	-	-
Hondorson	55	0.003	-	0.989	-	0.002	-	0.925	-
and Pabis	65	0.004	-	0.992	-	0.002	-	0.983	-
	75	0.005	-	0.986	-	0.003	-	0.858	-
Diffusion	55	0.003	-	1.00	-4.081	0.003	-	0.944	-0.664
	65	0.004	-	1.274	1.000	0.003	-	0.994	-1.950
	75	0.006	-	0.955	-1.268	0.008	-	0.594	0.055

Table 4. Effective Diffusion Coefficients of Pears at Different Temperatures

Drying Temperature (°C)	Non-Vacuum Impregnated Pears	Vacuum Impregnated Pears
	D_{eff} (m ² /s)	D_{eff} (m ² /s)
55	3.65×10 ⁻¹¹	2.7410-11
65	5.48×10 ⁻¹¹	3.6510-11
75	7.31×10 ⁻¹¹	4.5710-11

Model coefficients were determined by using MR values and SPSS 20.0 program for all selected models. Determined model coefficients were given in Table 3. The value of k in that table represents the drying rate constant. It can be clearly observed that this value is directly proportional to the drying temperature. That is the the higher drying temperature, the greater the k value. This constant is an indicator of drying rate. The rise in this value is an evidence for the increase in drying rate and the decline in drying time. Similar results were found by Simal et al., (2005) for kiwi fruit. The k parameter of the model increased with the increase of the drying air temperature of kiwi fruits for the whole range of temperatures studied.

Evaluation of Effective Diffusivity Coefficients and Activation Energy

The effective diffusivity coefficients (D_{eff}) was computed by plotting experimental drying data in terms of ln(MR) versus time (Lomauro et al.,1985; Doymaz and Akgün, 2009). The values of effective diffusivity coefficients were given in Table 4. Range of D_{eff} values were from 2.74×10^{-11} to 7.31×10^{-11} m²/s. The highest effective moisture diffusivity was obtained by the experiment performed at 75°C without vacuum impregnatiom process. It was observed that the effective diffusion coefficient increased as the temperature increased. The effective diffusion coefficient of non-vacuum impregnated pears was found to be larger than the vacuum impregnation pears' one.

In (D_{eff}) -1/T (absolute temperature in K) was plotted and the linearity of Arrhenius equation was shown in Figure 5. and Figure 6. The activation energy for the nonvacuum impregnated pears was 32.93 kJ / mol and the activation energy for the pears with vacuum impregnation was calculated as 24.25 kJ /mol. "Activation energy is an indication of the sensitivity of the diffusion to temperature. The high activation energy value shows that the effective diffusivity is highly sensitive to temperature (Kaymak-Ertekin. 2002). The effective diffusivity of non-vacuum impregnated samples has a higher sensitivity to temperature. These values are in fact consistent with those existing in the literature.



Figure 5. Arrhenius type relationship between effective Diffusivity (Deff) (m²/s) and Temperature (1/K) in nonvacuum impregnated pears

Ramirez et al. (2011) were found that the effect of vacuum impregnation on the effective diffusion coefficient was not significant and they found that the control group samples and the effective diffusion coefficient had similar values. Sahin and Ozturk (2016) were found effective diffusivity coefficient in between 2.75×10^{-10} and 10.25×10^{-10} . The activation energy for the non-vacuum impregnated pears was 34.68 (kJ/mol) and the activation energy for the pears with vacuum impregnation was calculated as 50.26 kJ / mol.

Conclusion

Pear samples was dried at constant air velocity of 1 m/s, different temperatures 55, 65 and 75°C and with and without vacuum impregnation until moisture content was reduced to under %15. Drying time of non-vacuum impregnated pears was determined as 640, 500 and 340 min and that for vacuum impregnated pears was determined as 700, 540 and 560 min respectively. It may be claimed that vacuum impregnation process had significant effect on drying times. Drying time of vacuum impregnated pears were higher than non vacuum impregnated pears. For the vacuum impregnated samples, external resistance across the drying were high because of the sugar content, especially at high temperatures. In accordance with the data related to drying, four kinetic models within drying model concept were evaluated. Experimental values were in accordance with the expected values resulted two empirical models (Page and Difussion) and hence the kinetic behaviour of with and without vacuum impregnated pears. The effective moisture difusivity was computed and it was determined that effective moisture diffusivity was directly proportional to drying temperature. Activation energy was also calculated 32.93 kJ / mol and 24.25 kJ / mol by the Arrhenius theory.

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Figure 6. Arrhenius type relationship between effective Diffusivity (Deff) (m²/s) and Temperature (1/K) in vacuum impregnated pears

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